

## ADAPTIVE ALGORITHM OF ROBUST CONTROL FOR NONLINEAR NONSTATIONARY SYSTEMS

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Essentially important desirable property of adaptive methods of synthesis of control algorithms is robustness, which, in this case, is understood as tolerance of results to changes of conditions of measuring. Robustness of algorithms is achieved by means of indemnification of disturbances to which influence the object of control is exposed. In the present paper the synthesis algorithm of robust control for nonlinear non-stationary systems with compensation of influence of disturbances and noises is offered by parametrical adaptation of a regulator and restoration of the current condition on previous.

Assume, that the mathematical model of functioning system is described by the system of nonlinear non-stationary difference equations of a kind [1]:

$$x(k+1) = \tilde{A}(k, x(k)) \cdot x(k) + \tilde{B}(k, x(k)) \cdot u(k), \quad x(0) = x_0, \quad (1)$$

where  $x(k)$  – the  $m$ -dimensional vector, which components define a state of the system in a step  $k$ ;  $u(k)$  –  $m$ -dimensional vector of control influences;  $\tilde{A}(k)$  – the matrix of parameters of object of control with  $(n \times n)$  dimension,  $\tilde{b}(k)$  – the matrix of influence of control with  $(n \times m)$  dimension;  $x_0$  – the initial condition of the system at the moment of time  $t_0$ ;  $(t_0, N)$  – the period of simulation; the step  $k$  corresponds to the moment of time  $t_k = t_0 + k \cdot \Delta t$ ,  $\Delta t$  – the period of quantization of a signal on time.

The cost function is [2]:

$$J = \int_{t_k}^{t_k + lp \cdot \Delta t} \left[ (x(t) - x_{\text{des.}}(t))^T \cdot Q_{\text{cr.}} \cdot (x(t) - x_{\text{des.}}(t)) + u^T(t) \cdot R_{\text{cr.}}^{-1} \cdot u(t) + u_{\text{opt.}}^T(t) \cdot R_{\text{cr.}}^{-1} \cdot u_{\text{opt.}}(t) \right] dt, \quad (2)$$

where  $[t_k, t_k + lp \cdot \Delta t]$  – sliding interval of optimization of predicting model of a kind:

$$\begin{aligned} x^m(j+1) &= \tilde{A}(k, x(k)) \cdot x^m(j) + \tilde{B}(k, x(k)) \cdot u(k), \quad x^m(j=k) = x(k), \\ j &= k, k+1, \dots, k+lp-1. \end{aligned}$$

In (2)  $Q_{\text{cr.}}$  – nonnegative matrix  $(n \times n)$ , a  $R_{\text{cr.}}$  – positive matrix  $(m \times m)$ ;  $x_{\text{des.}}$  – desired state of the system;  $u_{\text{opt.}}$  – optimum control, minimizing (2).

The length of the interval of optimization is calculated as follows [3]:

$$lp = 1 + \text{ceil} \left[ \text{norme}(\overset{\wedge}{A}(k) - \tilde{A}(k)) + \text{norme}(\overset{\wedge}{B}(k) - \tilde{B}(k)) \right],$$

where  $\text{ceil}$  – the function of a rounding off of value up to an integer,  $\text{norme}$  – Euclid's norm of a matrix; matrixes  $\overset{\wedge}{A}(k, \overset{\wedge}{x}(k))$ ,  $\overset{\wedge}{B}(k, \overset{\wedge}{x}(k))$  are calculated on a condition  $\overset{\wedge}{x}(k)$ , found in result of "run" of predicting model for one step.

$$\begin{aligned} \overset{\wedge}{x}(k) &= \overset{\wedge}{A}(k-1, \overset{\wedge}{x}(k-1)) \cdot \overset{\wedge}{x}(k-1) + \overset{\wedge}{B}(k-1, \overset{\wedge}{x}(k-1)) \cdot \overset{\wedge}{u}(k-1), \\ \overset{\wedge}{x}(0) &= x(0), \overset{\wedge}{A}(0, \overset{\wedge}{x}(0)) = \tilde{A}(0, x(0)), \overset{\wedge}{B}(0, \overset{\wedge}{x}(0)) = \tilde{B}(0, x(0)). \\ k &= 1, 2, \dots \end{aligned}$$

We synthesize the controller providing tracking property of the system to the set condition and a minimum of cost function (2). Control  $K(k)$  is defined as:

$$K(k) = R_{cr}^{-1} \cdot u_2(k),$$

where  $u_2(k)$  – the solution of system of difference equations in back time:

$$\begin{aligned} x^m(j-1) &= 2 \cdot x^m(j) - A(k, x(k)) \cdot x^m(j) - B(k, x(k)) \cdot u(k), & x^m(k+lp) &= x(k+lp), \\ u_1(j-1) &= A^T(k, x(k)) \cdot u_1(j) + \Delta t \cdot Q_{cr} \cdot (x^m(j) - x_{des.}(k)), & u_1(k+lp) &= x_{des.}(k+lp), \\ u_2(j-1) &= u_2(j) + B^T(k, x(k)) \cdot u_1(j) + \Delta t \cdot R_{cr} \cdot u(k), & u_2(k+lp) &= 0, \\ j &= k+lp, k+lp-1, \dots, k+1. \end{aligned}$$

Control value  $u(k)$  is searched as [4]:

$$u(k) = K(k) \cdot e^{\left[ \frac{norm}{\Delta t^2} \left( -sign \left( \sum_{i,j} (\hat{a}_{i,j}^{(k)} - \hat{\alpha}_{i,j}^{(k)}) \right) \right) \right]},$$

where  $norm = norme(\hat{A}(k) - \hat{A}(k)) + norme(\hat{B}(k) - \hat{B}(k))$ ,  $\hat{a}_{i,j}^{(k)}, \hat{\alpha}_{i,j}^{(k)}$  – elements of matrixes  $\hat{A}(k), \hat{A}(k)$  accordingly.

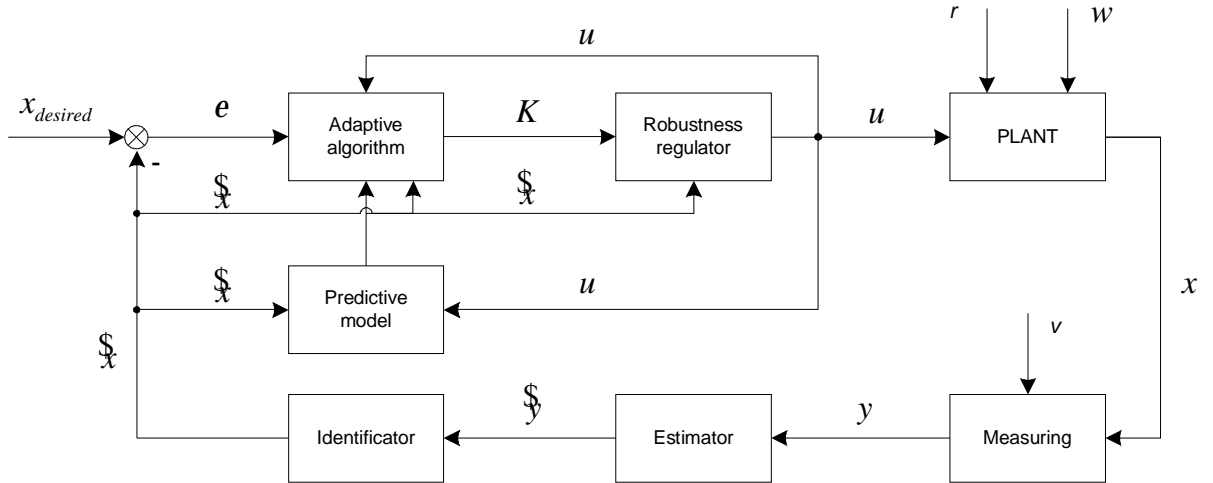


Fig. 1 – The Structure of an adaptive control system with robust regulator

On the fig. 1:  $r$  – not measured disturbances, influencing in the uncontrollable way on properties of object of control, i.e. on matrixes  $\hat{A}$  and  $\hat{B}$  of parameters of the system;  $w$  and  $v$  – randomize values, described as “mean-zero Gaussian noises”.

The measuring channel is described by the equation:

$$y(k) = C \cdot x(k) + v(k),$$

where  $C$  – the matrix of measuring channel with  $(m \times n)$  dimension.

The estimating of states of system and identification of its not measured parameters is realized by two in parallel working discrete Kalman's filters.

Let's present the equation (1) as:

$$x(k+1) = \Phi(x(k), u(k)) \cdot \Theta(k) + f(x(k), u(k)) + w(k),$$

where  $\Theta(\cdot)$  –  $n$ -dimensional vector, which includes non measured parameters.  
Thus the measuring channel becomes:

$$y(k+1) = C \cdot \left( \Phi(\hat{x}(k), u(k)) \cdot \Theta(k) + f(\hat{x}(k), u(k)) \right) + v(k).$$

The recursive algorithm for an estimation of states [2]:

$$\begin{aligned} \hat{x}(k+1) &= \hat{x}(k/k+1) + L(k) \cdot \left[ y(k+1) - C \cdot \hat{x}(k/k+1) \right], \\ \hat{x}(k/k+1) &= A(k, \Theta(k)) \cdot \hat{x}(k) + B(k, \Theta(k)) \cdot u(k) + w(k), \hat{x}(0) = x_0, \\ L(k) &= P_x(k/k+1) \cdot C^T \cdot \left[ C \cdot P_x(k/k+1) \cdot C^T + R \right]^{-1}, \\ P_x(k/k+1) &= A(k, \Theta(k)) \cdot P_x(k) \cdot A^T(k, \Theta(k)) + Q, \\ P_x(k+1) &= [I - L(k) \cdot C] \cdot P_x(k/k+1), \\ P_x(0) &= P_{x_0}. \end{aligned}$$

Here  $Q, R$  – covariance matrixes for noises  $w$  and  $v$  accordingly,  $I$  – identify matrix;  
 $\hat{x}(k/k+1)$  - is the estimate of  $x(k)$  given past measurements up to  $y(k-1)$ ;  $\hat{x}(k/k)$  is the updated estimate based on the last measurement  $y(k)$ .

In the block kind discrete Kalman's filter:

$$\begin{aligned} x(k+1/k) &= A(k, \hat{\Theta}(k)) \cdot (I - L(k) \cdot C) \cdot \hat{x}(k/k+1) + \left[ B(k, \hat{\Theta}(k)) \quad A(k, \hat{\Theta}(k)) \cdot L(k) \right] \cdot \begin{bmatrix} u(k) \\ y(k) \end{bmatrix}, \\ \hat{y}(k/k) &= C \cdot (I - L(k) \cdot C) \cdot \hat{x}(k/k+1) + C \cdot M \cdot y(k). \end{aligned}$$

Identification of parameters we will realize by following Kalman's filter:

$$\begin{aligned} \Theta(k+1) &= \Theta(k) + L(k) \cdot \left[ y(k+1) - C \cdot \Phi(\hat{x}(k), u(k)) \cdot \Theta(k) - C \cdot f(\hat{x}(k), u(k)) \right], \Theta(0) = \Theta_0, \\ L(k) &= P_\Theta(k) \cdot \Phi^T(\hat{x}(k), u(k)) \cdot M(k)^{-1}, \\ M(k) &= C \cdot \Phi(\hat{x}(k), u(k)) \cdot P_\Theta(k) \cdot \Phi^T(\hat{x}(k), u(k)) \cdot C^T + C \cdot Q \cdot C^T + R, \\ P_\Theta(k+1) &= \left[ I_n - L(k) \cdot C \cdot \Phi(\hat{x}(k), u(k)) \right] \cdot P_\Theta(k), \\ P_\Theta(0) &= P_{\Theta_0}. \end{aligned}$$

The developed algorithm has been used in the control system for controlling a speed of turning of blades of a propeller of a vessel. At sufficiently great speed of the ship turning of blades of a propeller with rated speed (1.8 degrees per second) result in sharp increase of torque in the diesel engine that is inadmissible as a safety matter. For functioning system with the set requirements (rates a torque of the engine is in allowable limits) also is necessary to take into account external disturbances (for example, influence of waves). Transients on a angle of turn of blades are performed on fig. 2.

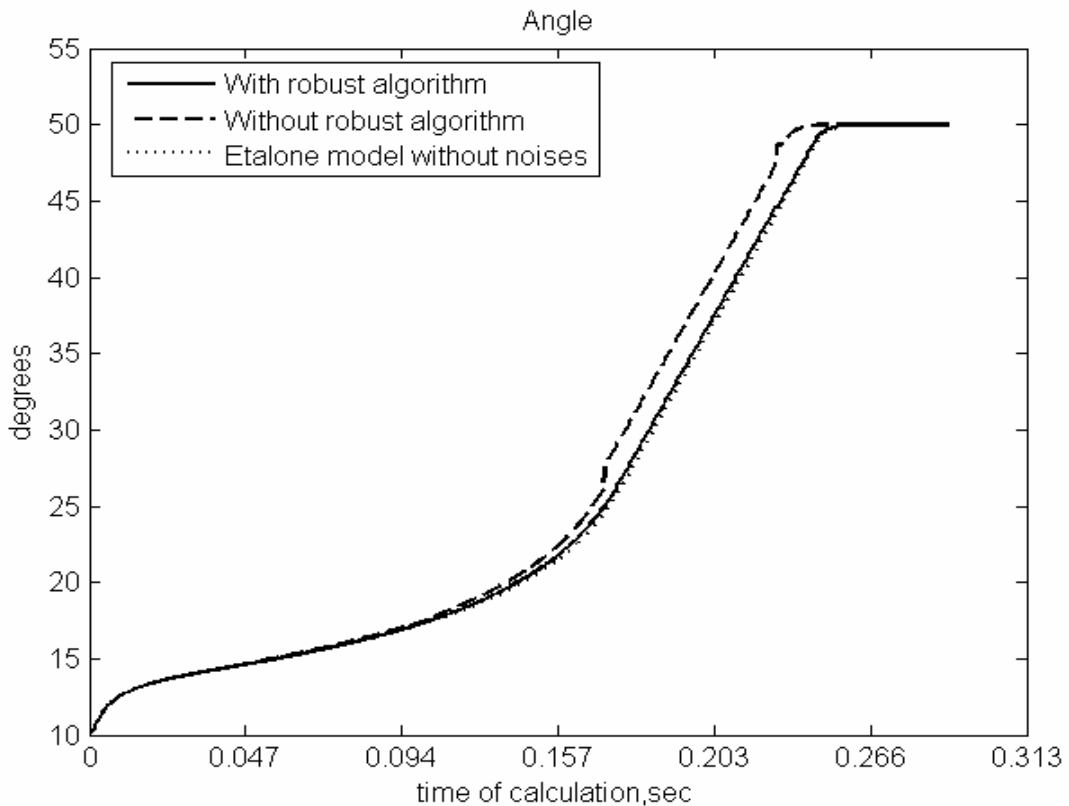


Fig. 2 – The result of simulation (angle of turning of propeller blades)

Estimations of a root-mean-square deviation of transients from a standard (etalon) trajectory are counted: 2.5353 for algorithm without robust regulator and 0.4174 - with it. According to the results, it is possible to conclude efficiency of the desired algorithm.

Still recently rough systems keeping the characteristics at deviations of parameters from settlement values were projected, as a rule, "to the touch" by simple selection of parameters at modeling as regular procedures of designing were not in most cases.

In the modern control theory more and more attention is given to sensitivity of algorithms for disturbances.

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